

ZULFAQAR Journal of Defence Science, Engineering & Technology

e-ISSN: 2773-5281 Vol. 3, Issue 1 (2020)

DOI: https://doi.org/10.58247/jdset-2020-0301-01

Journal homepage: https://zulfaqarjdset.upnm.edu.my



THE EFFECTS OF GROUND WATER LEVEL FLUCTUATION ON SLOPE STABILITY BY USING SLOPEW

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ARTICLE INFO	ABSTRACT
ARTICLE HISTORY	This study is a continuation of previous research work conducted by the author on
Received: 01-12-2019	the stability of man-made slope constructed in UPNM campus. This paper presents
Revised: 31-01-2020	the effects of ground water level (GWL) fluctuation on slope stability by using
Accepted: 28-02-2020	numerical simulation program, SlopeW. Ground water rises were simulated from
Published: 30-06-2020	5 m below the ground until 10 m above the ground. Soil samples were taken from
	the site and tested in laboratory and then were incorporated into the program. It
KEYWORDS	was found that the stability of the slope decreased with an increase of GWL. The
Factor of safety	critical slip surface formed by each case study is categorised as deep seated with
Ground water level	circular and non-circular shapes.
Fluctuation	
Slip surface	
SlopeW	

1.0 INTRODUCTION

Road developments on hilly areas often involve excavations, earthwork and slope construction. Slopes are cut and designed accordingly to comply with specific requirements to satisfy safety, stability and cost factors. In a tropical country like Malaysia, slope failures are common particularly during rainy season. It was reported that 28 major slope failures occurred between 1993-2011 and the death toll was more than 100 [1]. Although geotechnical engineers might have designed a safe slope, it remains a challenge to ensure its stability. The complexity of materials forming the slope [2-4], geological conditions [5] and hydrological system [6-7] are among the contributing factors influencing slope stability. Despite these, ground water level (GWL) greatly affects slope stability [8-9]. Considerable studies pertaining to GWL fluctuation in inducing slope failure have been conducted by researchers in recent years [10-11]. Many empirical and analytical equations were developed to analyze the relationship between slope failure and GWL quantitatively. However, most of the empirical and analytical research were focused on specific slope regions and only considered limited parameters. With the advent of computer technology nowadays, numerical simulation programs have become a powerful tool and are widely used by researchers due to their capability to solve complicated computation problems [12]. Nonetheless numerical simulation can provide more accurate results in comparison to analytical methods.

This research is a continuation of previous work conducted by the author pertaining to stability of man-made slope constructed in UPNM campus [13]. There were five different slopes constructed along the road and only one was selected for investigation as shown in Figure 1. This slope was located at the highest point among others as well as the steepest. Field survey was carried out to determine the existing ground water table and seepage location. Previous research had determined the safety factor of the slope without taking into consideration the GWL fluctuation. In this paper, further analysis was conducted to study the effects of GWL rising and to determine the shape of slip surface formation. The laboratory data presented in this paper were obtained from the local soil and then were incorporated into numerical simulation program, SlopeW.



Figure 1. Slope construction in UPNM campus [13]

2.0 METHODOLOGY

The methodology of this research was divided into two parts. The first part was laboratory work. Disturbed and undisturbed soil samples were taken at the top and bottom of the slope to determine the types of soil and shear strength properties. For sieve analysis, test and samples preparation were carried out as stated in BS1377: Part 2:1990. British Soil Classification System (BSCS) was used to classify the types of soil. Meanwhile, for soil shear strength determination, Automated Direct Shear Test machine was used as shown in Figure 2.

The second part of this research was to conduct numerical simulation analysis by using SlopeW program. Two analyses were carried out including the determination of the safety factor of the slope due to GWL fluctuation and identify slip surface formation. The geometry of slope model set up is shown in Figure 3, which consists of nine berms. The estimated slope height and slope inclination angle were approximately 22 m and 70 ° respectively. All the units and scales used in the program were in meter and kilo newton. Two different types of soil layer, namely the upper and lower soil were constructed to replicate the actual site condition. The soil parameters for both layers were obtained from the laboratory test and assigned in the SlopeW program. The laboratory test data are tabulated in Table 1. The assumed GWL was initially setup at 5 m below the ground (recorded as 1 m) as shown in Figure 3. The GWL was then increased to 1 m interval. Therefore, the variation of GWL used in this study was assumed at level 1 m until 15 m. The Factor of Safety (FOS) of slope for each GWL increment was computed by using the Morgenstern-Price method.

Table 1. Soil parameters for upper and lower soil layers assigned in SlopeW							
Depth (m)	Soil	Cohesion, c	Angle of	Unit weight,	Colour		
	Layer	(kN/m^2)	friction, θ°	γ (kN/m ³)	Legend		
0 - 13	Upper	16	21	16	Yellow		
13 - 22	Lower	13	23.3	17	Green		

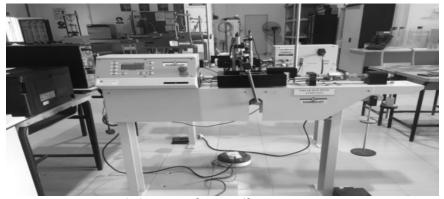


Figure 2. Automated Direct Shear Test apparatus

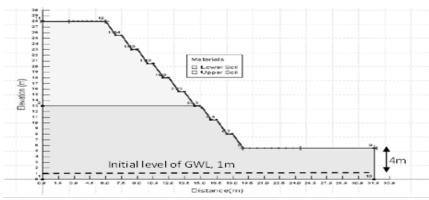


Figure 3. Geometry of slope model set up in SlopeW

3.0 RESULTS AND DISCUSSIONS

The particle size distribution for both soil layers is shown in Figure 4. According to British Soil Classification System, the soil is classified as sandy slit and silty sand for upper and lower soil layer respectively.

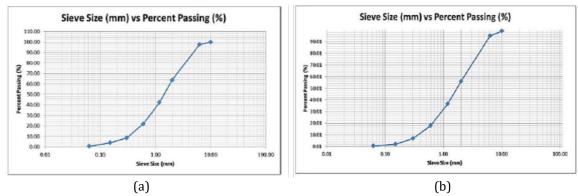


Figure 4. Sieve analysis results (a) upper soil layer is classified as sandy silt (b) lower soil layer is classified as silty sand

There are nine undisturbed soil samples were tested to determine the shear strength properties for both soil layers. The average results are shown in Figure 5 and Table 1.

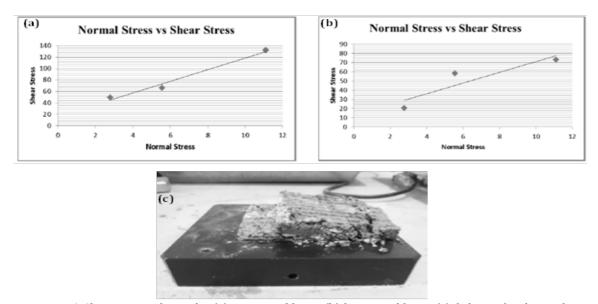


Figure 5. Shear strength results (a) upper soil layer (b) lower soil layer (c) failure of soil sample

The influence of GWL rise upon FOS is presented in Figure 6. The GWL was simulated for each 1 m height increment, and it was started from 5m below the ground. The 1 m to 5 m heights of GWL depicted in the Figure 6 indicate water level below the ground. Meanwhile, 6 m to 15 m heights are water level above the ground. The highest FOS value obtained from SlopeW was 0.733 for water level height of 5 m below the ground (the farthest GWL). A further increase of GWL resulted in the decrement of FOS. The decrement was noticeable for the GWL between 1 m to 5 m below the ground. However, no significant changes were observed when the GWL increased every 1 m height above the ground. The overall FOS values were lesser than 1 regardless of any water level heights carried out in this study. This indicates instability condition for the slope and eventually, with the presence of GWL at any level could potentially cause slope failure or landslide. This finding is similar with previous studies that showed that the FOS decreased when GWL rose, and the decrement declined dramatically when water height reached critical depth [14].

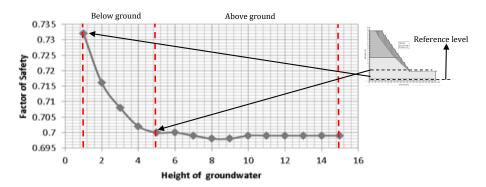


Figure 6. GWL influence on FOS of slope

Figure 7 shows the formation of critical slip surface for different GWL heights located below the ground. For all case studies, as the GWL increases to ground level, the shape of slip surface tends to become semi-circular and have relatively thicker soil mass. The slip surface line was observed passing through the crest of slope and extended to the toe. This type of failure is categories as deep-seated failure with circular shape. Deep-seated failure may induce large scale soil failure that can cause remarkable damage. For GWL in case (a), the slip surface is much thinner as compared to other cases. This is expected to be due to GWL being located at the farthest and FOS the highest.

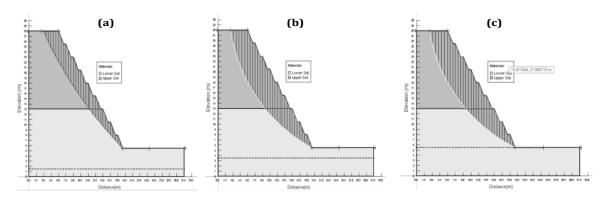


Figure 7. Critical slip surface formation for GWL heights below the ground (a) 5 m (b) 3 m (c) 0 m

Figure 8 shows the critical slipe surface for GWL rising above the ground. As the GWL increases, the slip surface tends to lie close to the slope surface and the line is not circular. This can be explained due to FOS having small changes through the cases (b) to (e). This is supported by the graph shown in Figure 6.

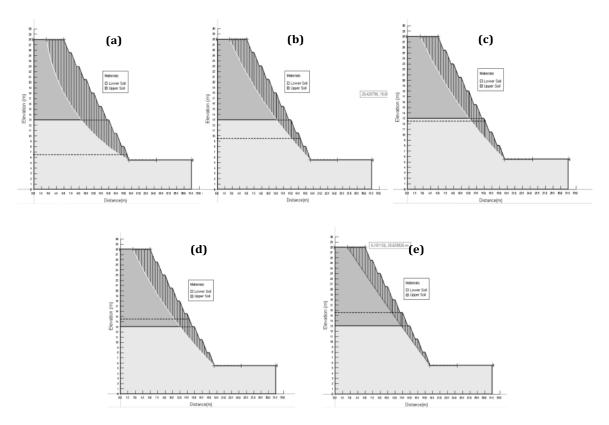


Figure 8. Critical slip surface formation for GWT heights above the ground (a) 1 m (b) 4 m (c) 7 m (d) 9 m (e) 7 m

4.0 CONCLUSION

Stability analysis of man-made slope due to GWL fluctuation is studied in which the effects of GWL fluctuation was carried out by using SlopeW program. It was found that the stability of slope decreased with increase of GWL. The critical slip surface formation has an influence on GWL increment. For all case studies, the slip surface formation is categorised as deep seated regardless of any increment of GWL height. The circular slip line with thick soil mass occurred when GWL rose from below the ground. However, the non-circular slip line was formed for the case where ground water rose above the ground.

5.0 ACKNOWLEDGEMENT

The authors appreciate the financial support by the National Defence University of Malaysia under grant no. UPNM/2019/GPJP/TK/5.

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